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# LINEAR INTEGRATED CIRCUITS

## PART-06

### Constant Current Biasing Techniques for Differential Amplifiers

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# Constant Current Biasing - Outline

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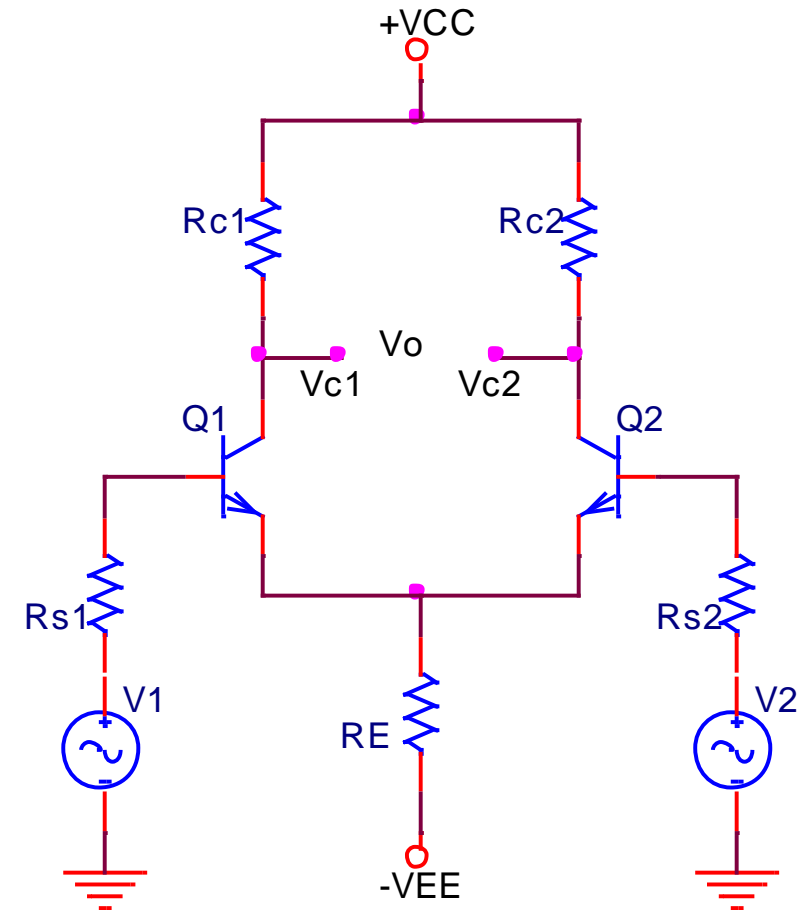
1. Why constant current biasing?
2. Constant current biasing techniques
  - Simple basing
  - PN diode based biasing
  - Zener diode based biasing
  - Current mirror based biasing
3. Summary

# Why Constant Current Biasing?

- Operating point currents in Differential Amplifiers

$$I_{E1} = I_{E2} = \frac{V_{EE} - V_{BE}}{(R_S/\beta + 2R_E)}$$

- Depends upon  $\beta$  that change with transistor.
- Depends upon  $V_{BE}$  that change with temperature.
- To remove these dependencies
  - Increase  $R_E$  leads to increase in CMRR but reduces  $I_E$
  - Increase  $I_E$ , we have to increase  $V_{EE}$
- Alternatively, Constant Current Biasing is used



Refer: Part-03 DC Analysis of BJT Differential Amplifiers

# Constant Current Biasing – Simple

Voltage at the base terminal of  $Q_3$  is given as

$$V_{B3} = \frac{-V_{EE}}{R_1 + R_2} R_2$$

Since,  $V_{BE} = V_B - V_E$ ,

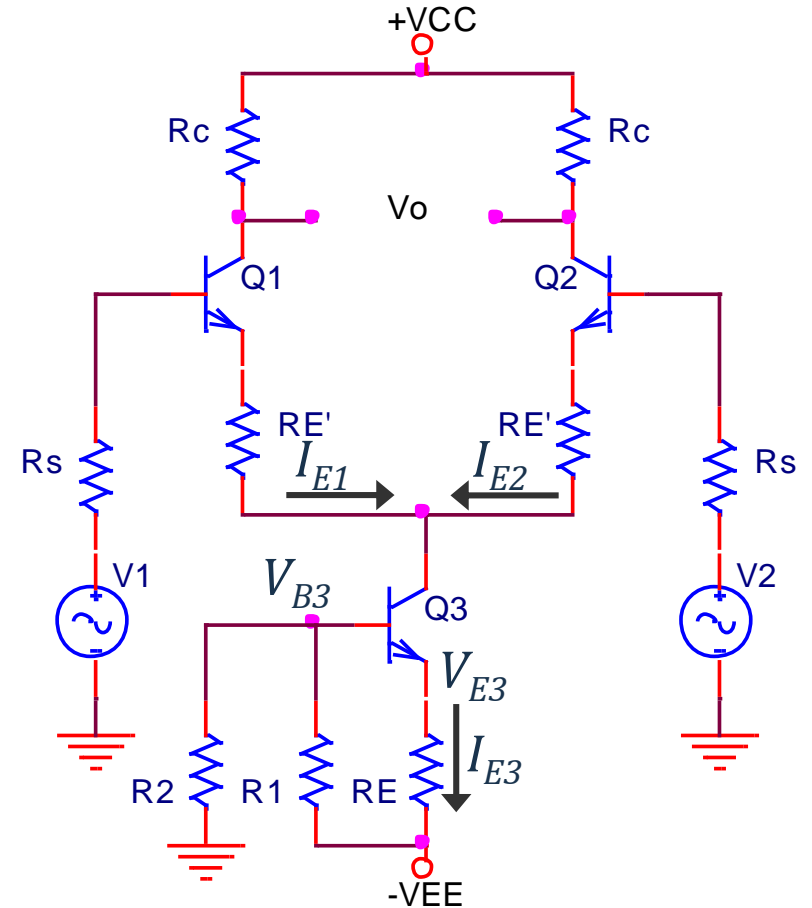
$$V_{E3} = V_{B3} - V_{BE3} = -\frac{V_{EE}}{R_1 + R_2} R_2 - V_{BE3} \quad (1)$$

Current through  $R_E$  is

$$I_{E3} = \frac{V_{E3} - (-V_{EE})}{R_E} = \frac{1}{R_E} (V_{EE} + V_{E3})$$

Put  $V_{E3}$  from (1)

$$I_{E3} = \frac{1}{R_E} \left( V_{EE} - \frac{R_2}{R_1 + R_2} V_{EE} - V_{BE3} \right) = I_{C3}$$



# Constant Current Biasing – Simple

Due to symmetrical circuitry

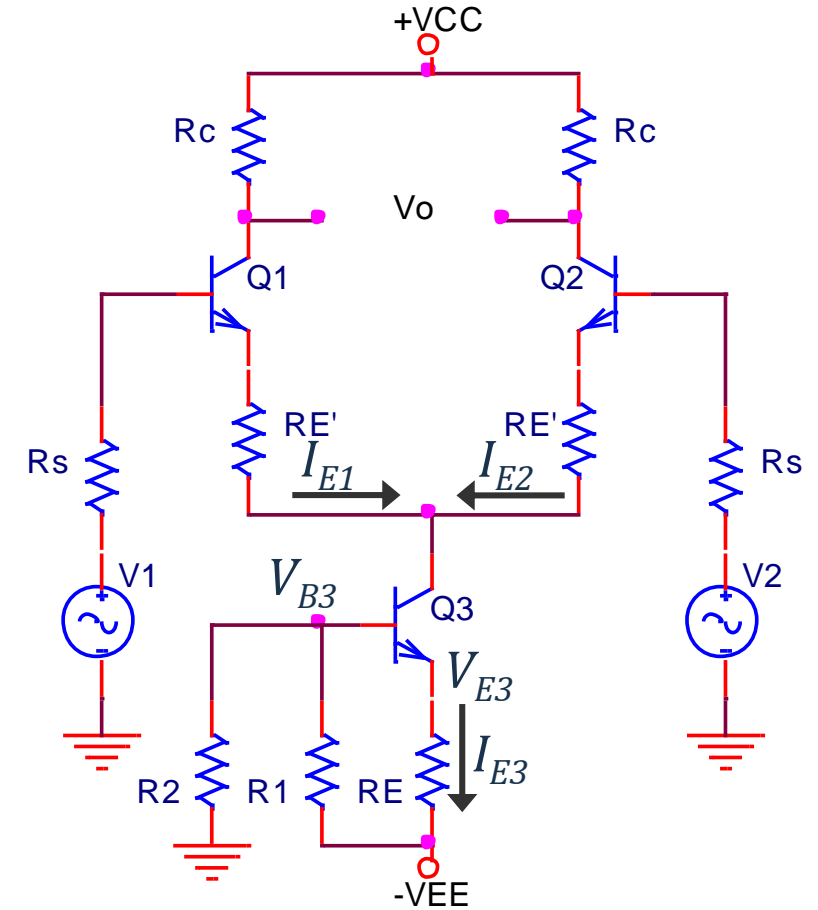
$$I_{E1} = I_{E2} = \frac{I_{C3}}{2}$$

$$I_{E1} = I_{E2} = \frac{1}{2R_E} \left( V_{EE} - \frac{R_2}{R_1 + R_2} V_{EE} - V_{BE3} \right)$$

Hence, currents in  $Q_1$  and  $Q_2$  do not depend on  $\beta$

However, still dependent upon  $V_{BE3}$  whose value decreases @  $2\text{mV}/^\circ\text{C}$ .

Let's now consider biasing for thermal stability.



# Constant Current Biasing - PN Diode

Thermal stability of the circuit can be increased with a diode, if placed in series with  $R_1$ .

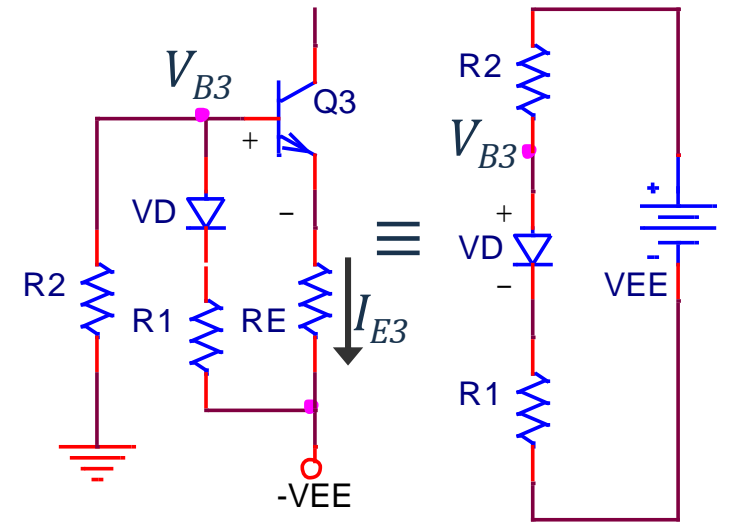
From base voltage  $V_{B3}$  using KVL

$$V_{B3} = (V_{EE} - V_D) \frac{R_1}{R_1 + R_2} + V_D \text{ and } V_{B3} = V_{BE3} + I_{E3} R_E$$

$$(V_{EE} - V_D) \frac{R_1}{R_1 + R_2} + V_D = V_{BE3} + I_{E3} R_E$$

$$I_{E3} = \frac{1}{R_E} \left( \frac{V_{EE} R_1}{R_1 + R_2} + V_D - \frac{V_D R_1}{R_1 + R_2} - V_{BE3} \right)$$

$$I_{E3} = \frac{1}{R_E} \left( \frac{V_{EE} R_1}{R_1 + R_2} + \frac{V_D R_1 + V_D R_2 - V_D R_1}{R_1 + R_2} - V_{BE3} \right)$$



# Constant Current Biasing - PN Diode

After simplification

$$I_{E3} = \frac{1}{R_E} \left( \frac{V_{EE}R_1}{R_1 + R_2} + \frac{V_D R_2}{R_1 + R_2} - V_{BE3} \right)$$

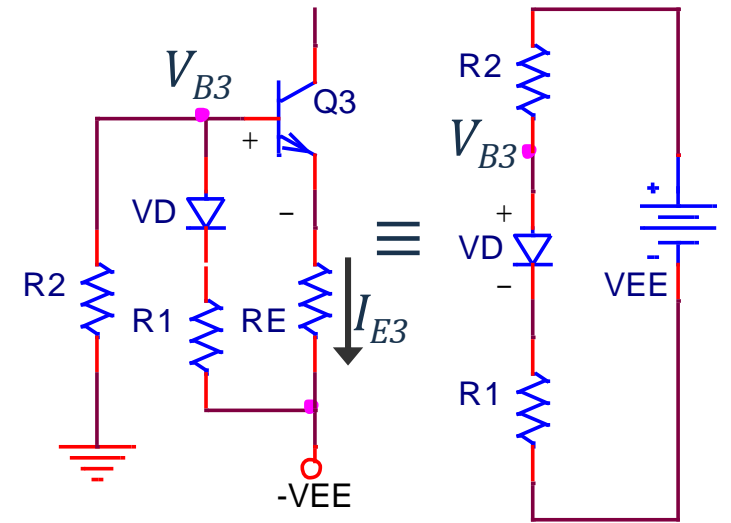
Adjust  $R_1$  and  $R_2$  so that

$$V_{BE3} = \frac{V_D R_2}{R_1 + R_2} \quad (2)$$

$$I_{E3} = \frac{1}{R_E} \frac{V_{EE} R_1}{R_1 + R_2}$$

$$I_{E1} = I_{E2} = \frac{I_{E3}}{2} = \frac{1}{2R_E} \frac{V_{EE} R_1}{R_1 + R_2}$$

The effect of temperature in the form of voltage variation in transistor is cancelled by diode.



# Constant Current Biasing - Zener Diode

Zener diodes may be used in place of diodes.

$$V_{B3} = V_Z - V_{EE}$$

$$V_{E3} = V_{B3} - V_{BE3}$$

$$V_{E3} = V_Z - V_{EE} - V_{BE3}$$

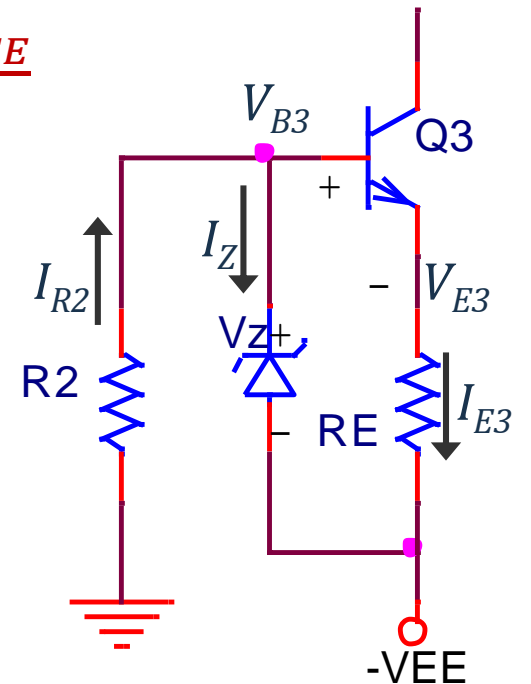
However, 
$$I_{E3} = \frac{V_{E3} + V_{EE}}{R_E}$$

$$I_{E3} = \frac{V_Z - V_{EE} - V_{BE3} + V_{EE}}{R_E} = \frac{V_Z - V_{BE3}}{R_E}$$

$$I_{E1} = I_{E2} = \frac{I_{E3}}{2} = \frac{V_Z - V_{BE3}}{2R_E}$$

Resistance  $R_2$  is adjusted make Zener diode conduct in reverse bias, i.e.,  $I_{R2} = 1.2I_{Z(min)}$

$$R_2 = \frac{V_{B3}}{I_{R2}} = \frac{V_Z - V_{EE}}{I_{R2}}$$





# Constant Current Biasing - Current Mirror

Circuit in which output current is forced to equal input current is called a Current Mirror circuit.

$Q_3$  and  $Q_4$  are identical, therefore

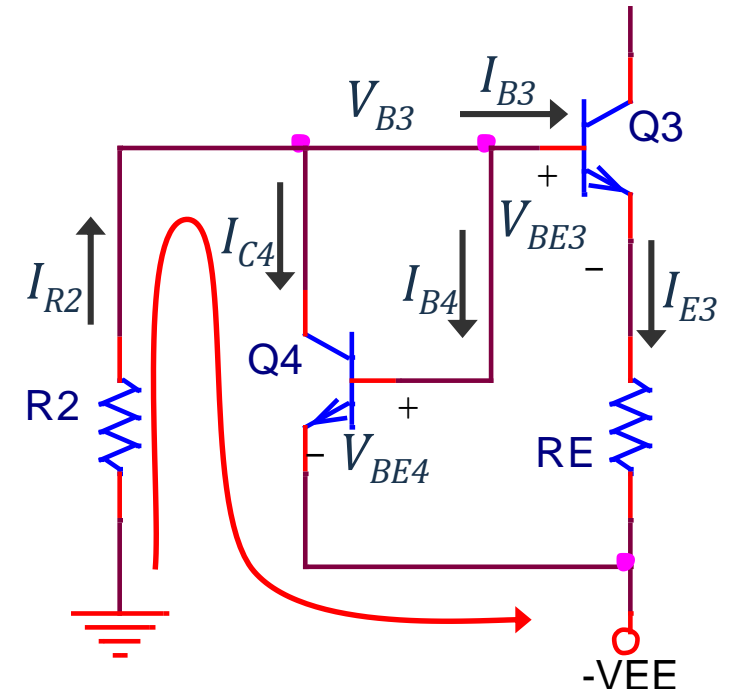
$$I_{B3} = I_{B4}, I_{C3} = I_{C4} \text{ and } V_{BE3} = V_{BE4}$$

Apply KCL at node  $V_{B3}$

$$I_{R2} = I_{C4} + I_{B3} + I_{B4} = I_{C3} + 2I_{B3}$$

$$I_{R2} = I_{C3} + 2 \frac{I_{C3}}{\beta} = I_{C3} \left( 1 + \frac{2}{\beta} \right) \approx I_{C3}$$

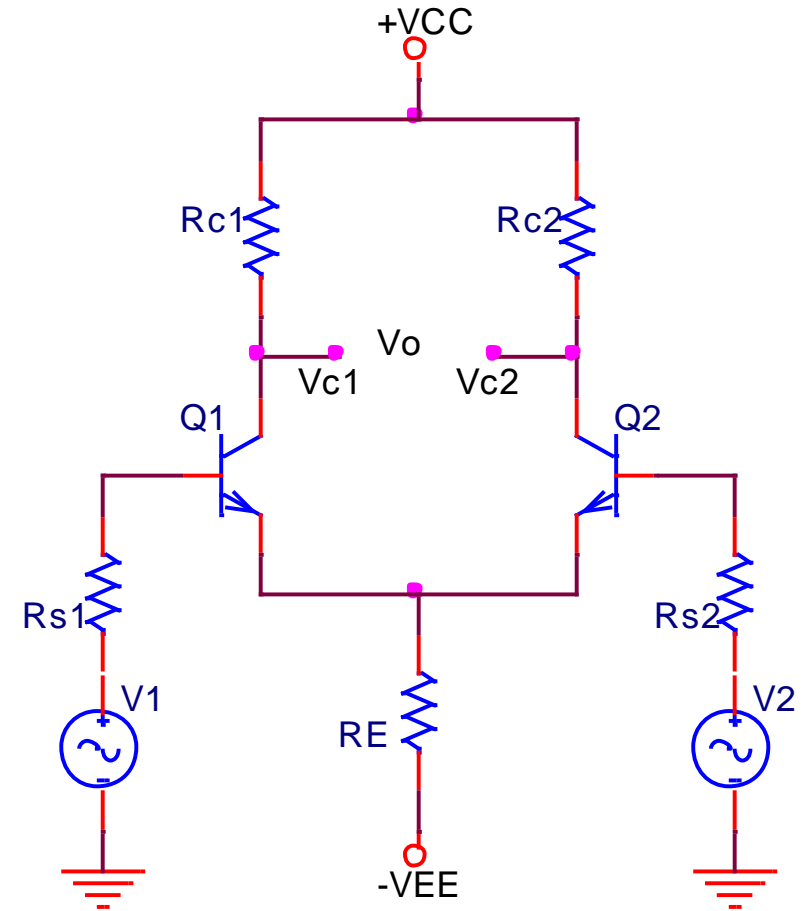
$$I_{R2} = I_{C4} = \frac{V_{BE} - V_{EE}}{R_2} = I_{E3}$$



# Summary - Constant Current Biasing

Operating Current **without** Constant Current Biasing

$$I_E = \frac{V_{EE} - V_{BE}}{(R_S/\beta + 2R_E)}$$



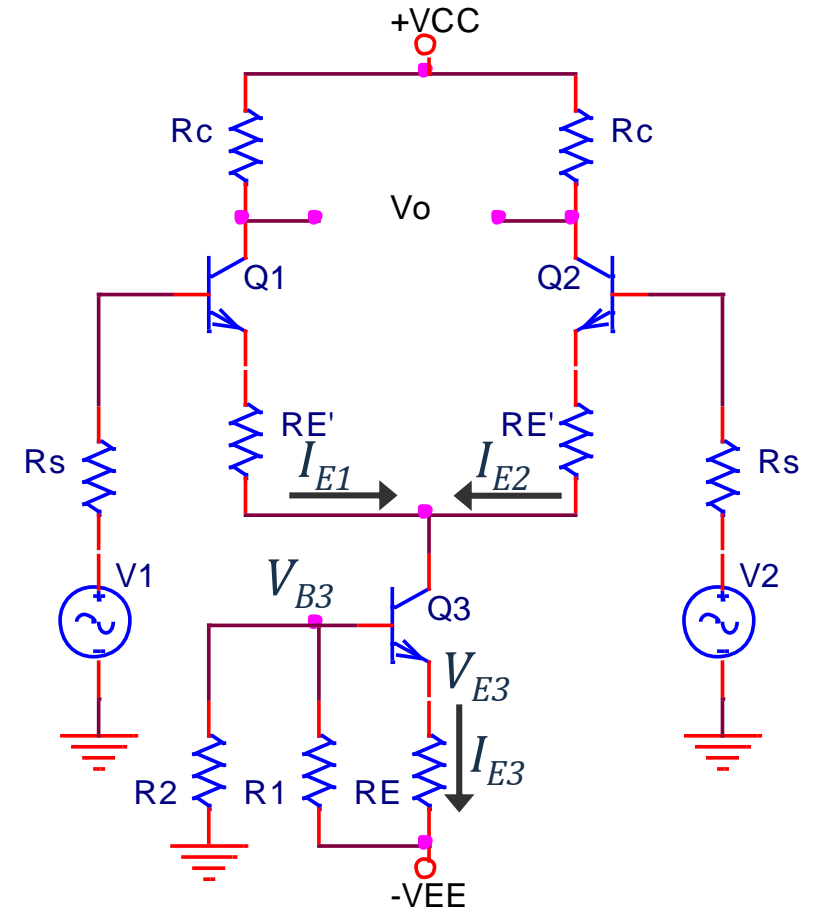
# Summary - Constant Current Biasing

Operating Current without Constant Current Biasing

$$I_E = \frac{V_{EE} - V_{BE}}{(R_s/\beta + 2R_E)}$$

(1) Simple Biasing

$$I_E = \frac{V_{EE} - \frac{R_2}{R_1 + R_2} V_{EE} - V_{BE3}}{2R_E}$$



# Summary - Constant Current Biasing

Operating Current without Constant Current Biasing

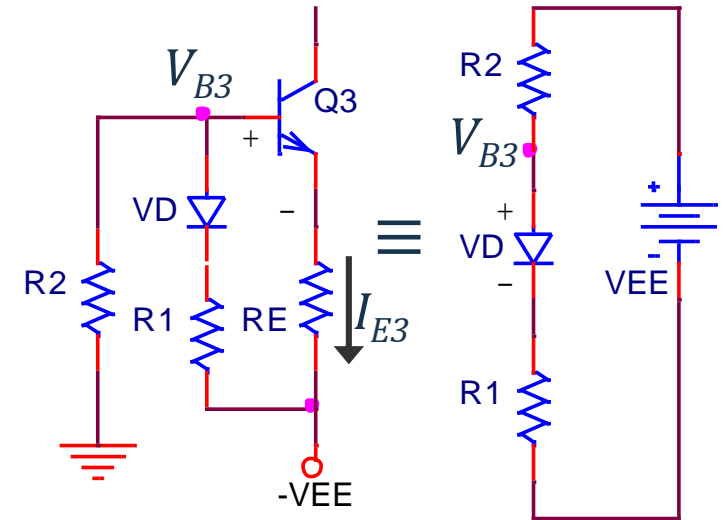
$$I_E = \frac{V_{EE} - V_{BE}}{(R_S/\beta + 2R_E)}$$

(1) Simple Biasing

$$I_E = \frac{V_{EE} - \frac{R_2}{R_1 + R_2} V_{EE} - V_{BE3}}{2R_E}$$

(2) PN Diode Biasing ( $V_{BE3} = \frac{V_D R_2}{R_1 + R_2}$ )

$$I_E = \frac{1}{2R_E} \frac{V_{EE} R_1}{R_1 + R_2}$$



# Summary - Constant Current Biasing

Operating Current without Constant Current Biasing

$$I_E = \frac{V_{EE} - V_{BE}}{(R_s/\beta + 2R_E)}$$

(1) Simple Biasing

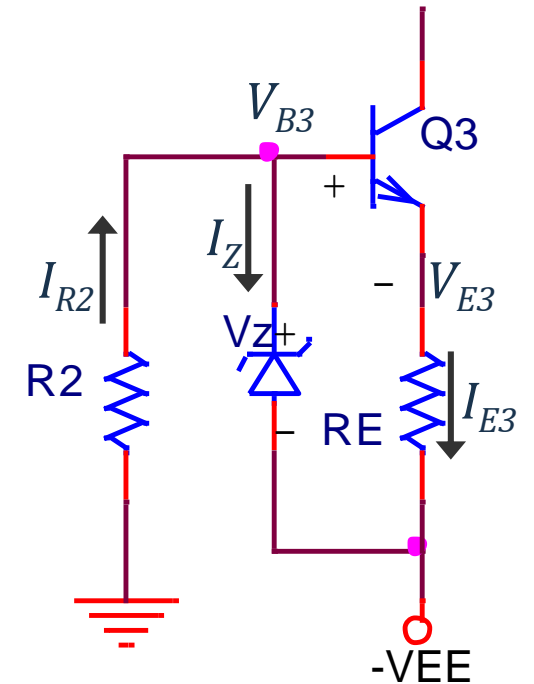
$$I_E = \frac{V_{EE} - \frac{R_2}{R_1 + R_2} V_{EE} - V_{BE3}}{2R_E}$$

(2) PN Diode Biasing

$$I_E = \frac{1}{2R_E} \frac{V_{EE} R_1}{R_1 + R_2}$$

(3) Zener Diode Biasing

$$I_E = \frac{V_Z - V_{BE3}}{2R_E}$$



# Summary - Constant Current Biasing

Operating Current without Constant Current Biasing

$$I_E = \frac{V_{EE} - V_{BE}}{(R_S/\beta + 2R_E)}$$

(1) Simple Biasing

$$I_E = \frac{V_{EE} - \frac{R_2}{R_1 + R_2} V_{EE} - V_{BE3}}{2R_E}$$

(2) PN Diode Biasing

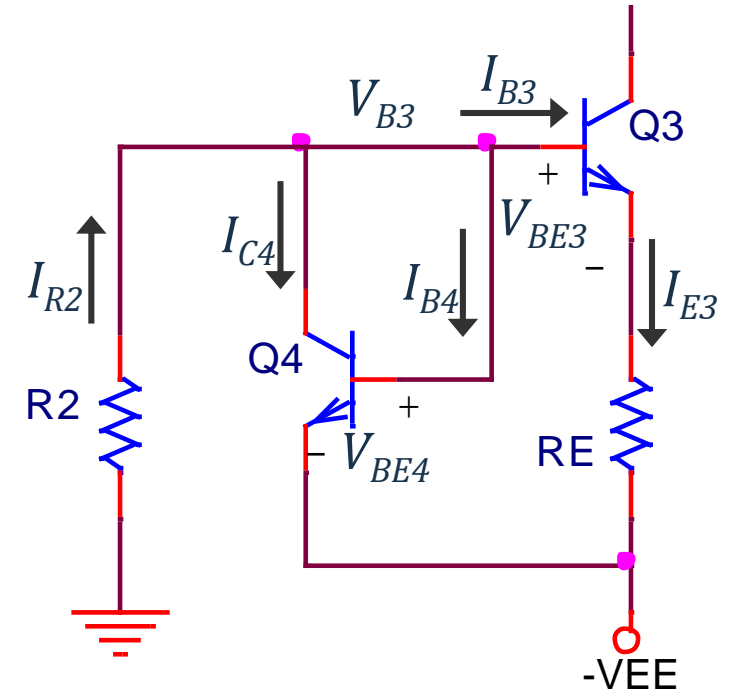
$$I_E = \frac{1}{2R_E} \frac{V_{EE} R_1}{R_1 + R_2}$$

(3) Zener Diode Biasing

$$I_E = \frac{V_Z - V_{BE3}}{2R_E}$$

(4) Current Mirror Biasing

$$I_E = \frac{V_{BE} - V_{EE}}{2R_2}$$



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# Thank You

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